Drying can be defined as a unit operation in which a liquid-solid separation is accomplished by the supply of heat, with separation resulting from the evaporation of liquid. Although in the majority of cases water is the liquid being removed, solvent evaporation is also encountered. The definition may be extended to include the dehydration of food, feed, and salts, and the removal of hydroxyl groups from organic molecules.

This book is based on my personal experience gained in the selection and operation of drying equipment while employed by Akzo Nobel, a multinational company that manufactured, at that time, bulk and fine chemicals, pharmaceuticals, and coatings. Since 2000, I gained experience while working as an independent consultant.

Laboratory measurements and investigations concerning the drying of a product should be the first stage of the selection of a new dryer or the replacement of one. This aspect is discussed in Chapter 3. During the next stage, a person should seek the cooperation of a reputable dryer manufacturer. Close cooperation between the manufacturer and the potential user is essential, because one partner is knowledgeable about the equipment and the other person has expertise regarding the product. Since small-scale testing of drying equipment can be carried out, such testing can provide valuable insight into ultimate dryer selection. However, it is important that each partner have some insight into the other's field so that the user can develop value judgments on the equipment being recommended by the manufacturer. The size of the equipment must be checked, using various techniques (e.g., estimating methods, rules of thumb, rough-and-ready calculations). This book covers these techniques for each class of dryer.

Drying in the Process Industry, First Edition. C.M. van 't Land.

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Various reasons exist for drying materials to a specific level or range:

- 1. It is often necessary to obtain a free-flowing material that can be stored, packed, transported, or dosed.
- 2. Contractual limits exist for many products (e.g., salt, sand, yarn).
- 3. Statutory limits are in force for some materials (e.g., tobacco, flour).
- 4. A moisture content within a specified range may have to be obtained for quality control purposes. For many dried foods and feeds, too much moisture may adversely affect shelf life and nutritional value, whereas a moisture content too low, due to overdrying, may cause the loss of valuable nutrients. Moisture contents that are either too high or too low may render a product less enjoyable.
- 5. The feasibility of subsequent process steps sometimes requires that the moisture content be between specified limits, as in the milling of wheat or the pressing of pharmaceutical tablets. Another example is the low moisture content of rubber chemicals to be used in the vulcanization process of tires. Too much moisture causes the formation of blisters.
- 6. The onset of mildew and bacterial growth in such textiles as woolen cloth can be prevented by drying the cloth to a specific moisture content.
- 7. A drying step can be used as a shaping step. The manufacture of fluid cracking catalysts is an example. A spray-drying step produces hard and dry spheres of average diameter 80 μm. However, next, the spheres are leached with water to remove sodium salts. That step is followed by filtration and flash drying.

Typical dryer feeds are:

- 1. Objects (e.g., bricks)
- 2. Particulate materials (e.g., sodium sulfate crystals)
- 3. Filter and centrifuge cakes
- 4. Sheet material (e.g., paper for newspapers)
- 5. Pastes (e.g., dibenzoyl peroxide paste)
- 6. Liquids (i.e., solutions, emulsions, or suspensions)

Drying is an energy-intensive process. In general, heating and evaporation require large quantities of energy. An apple of mass 100 g hanging 4 m above the ground has a potential energy of approximately 4 J. Heating 1 kg of water from 15°C to 100°C requires 356,150 J. Evaporating 1 kg of water at 100°C and atmospheric pressure requires 2,285,000 J. Thus, in terms of energy, thermal effects are in general much more important than mechanical effects. This explains why the energy consumption in phase transformation and the heating in a drying operation exceeds the energy consumption of electromotors. In this respect, there is one more important aspect. The energy to evaporate 1 kmol of liquid is approximately constant for all liquids. Thus, it is possible to evaporate 18 kg of water (which has a kilomolecular weight of

18 kg·kmol⁻¹) with this heat of evaporation. However, it is also possible to evaporate 92 kg of toluene (which has a kilomolecular weight of 92 kg·kmol⁻¹) with this amount of heat. The explanation is that kilomoles of different substances contain the same number of molecules: $6.023 \cdot 10^{26}$ (Avogadro's number). Thus, on evaporating

1 kmol of a substance, the bonds between this number of molecules must be broken. The bonds between the molecules are relatively weak Van der Waals forces and are approximately equal. The evaporation of water occurs more frequently than the evaporation of organic liquids.

The energy consumption of the drying operation in the UK has been reviewed by Bahu and Kemp [1]:

- The energy consumption of drying is 8% of the industrial energy consumption. The industrial energy consumption comprises both processes and buildings.
- The annual water evaporation amounts to $2 \cdot 10^{10}$ kg. This is equivalent to 100-m water columns on 27.2 soccer fields (70·105 m²). As the U.S. economy is about 5.5 times larger than the UK economy, the annual water evaporation in the United States due to drying could be $1.1 \cdot 10^{11}$ kg.
- In 1981, drying required $1.622 \cdot 10^{14}$ kJ. This figure was possibly 10 to 20% lower in 1991.
- $(1.622 \cdot 10^{14})/(2 \cdot 10^{10}) = 8110 \text{ kJ}$ per kilogram of evaporated water. This consumption figure includes electricity. Excluding electricity, the consumption figure is possibly 7000 kJ·kg⁻¹. Compared to the heat of evaporation of water at 0°C and atmospheric pressure (i.e., 2500 kJ·kg⁻¹), the consumption figure is quite high. In the chapters to come, the background of this state of affairs is discussed.
- Annual costs are determined by taking 32,000 kJ·nm⁻³ as the lower heating value of natural gas. The lower heating value is relevant if the heat of condensation of the water vapor in the combustion gases is not recovered. In the UK, an industrial price of €0.30 is typical:

$$\frac{1.622 \cdot 10^{14} \cdot 0.30}{32,000} = \pounds 1,520,625,000$$

These calculations illustrate that drying is an expensive means of accomplishing a liquid–solid separation; as a rule of thumb, 2 to 3 kg of steam is required for the evaporation of each kilogram of water. In a four-effect evaporation plant, approximately 4 kg of water can be evaporated with 1 kg of steam. Furthermore, performing a solid–liquid separation by means of a centrifuge or filter is usually much cheaper than using a dryer. Calculations concerning the energy required by the drying process begin with an assessment of the enthalpy difference between the process flows leaving the dryer and the process flow entering the dryer. Enthalpy differences are heat effects at constant pressure. In convective drying processes, the drying gas should be excluded from these calculations. Thus, the net heat is arrived at.

The heat required for drying can be supplied by the fundamentally different mechanisms of convection, conduction, and radiation:

- 1. *Convection.* A carrier gas (usually, air) supplies the heat for the evaporation of the liquid by the conversion of sensible heat into latent heat. The carrier gas subsequently entrains the volatile matter.
- 2. *Conduction.* The heat is supplied indirectly and the carrier gas serves only to remove the evaporated liquid. Typically, the airflow is approximately 10% of the airflow used in a convective process. Conduction of heat is the heat transport mechanism at contact drying.
- 3. *Radiation.* This type of drying can, in principle, be *nonpenetrating*, such as the drying of paint by infrared radiation, or *penetrating*, such as the drying of food or pharmaceuticals by dielectric drying. Dielectric drying (radio-frequency drying and microwave drying) is the only process in which heat is developed in the material being dried rather than having heat diffused into the material. Again a carrier gas is required to remove the evaporated liquid.

A combination of two mechanisms may be encountered in some dryer types.

The situation in the United States was analyzed by Strumillo and Lopez-Cacicedo [2], who found that 99% of dryer energy consumption could be attributed to six dryer types. In order of importance:

- Flash dryer
- Spray dryer
- Cylinder dryer for paper
- Convective rotary dryer
- Contact rotary dryer
- Fluid-bed dryer

This list illustrates that in terms of tonnage, convective drying is more important than conduction (contact) drying.

Dryer Types

A great variety of dryer types is commercially available. The reasons are as follows:

- Different products have very different drying times.
- The product quality often requires a certain dryer type or mode.
- It is often necessary to transport particulate material through a dryer.

A distinction should be made between free and bound moisture. Initially, *free water* is evaporated until the critical moisture content is reached. Free water's latent heat of evaporation is essentially equal to that of water on evaporating from a pool,

with the heat transfer being the rate-determining step. Evaporation occurs at a constant rate if the heat supply is constant. Thus, as long as there is free water, the rate of evaporation is not a function of the water concentration. The order of the process is then zero. Drying to below the critical moisture content requires the evaporation of bound water, with the evaporation rate decreasing if the heat supply is kept constant. *Bound water* can be present in pores or crevices, can be physically absorbed, or can be present as water of hydration. The latent heat of evaporation of bound water is usually higher than that of free water; for example, the ratio of the latent heats of evaporation of water in wool containing 16 and 30% water by weight (the latter value is the critical moisture content) is approximately 1.1:1.

Temperature and Moisture Profiles

In this book we deal only with phenomena related to objects to be dried. Thus, transient temperature and moisture profiles in the product to be dried are not discussed.

Drying Systems

Unlike a centrifuge, for example, a dryer consists of a number of pieces of equipment grouped together in a subsystem. It is therefore more correct to refer to drying *systems*. Convective drying systems are often more extended than contact or radiation dryer systems. Drying is often the last process step, which is followed by a solids-handling system designed by mechanical engineers. In addition, being an energy-intensive process, drying is sometimes handled by energy specialists. It can therefore be considered a unit operation that falls at the interface of three disciplines: chemical, mechanical, and energy engineering.

In Chapter 2 it is recommended that the drying step not be considered in isolation but rather be reviewed in the context of the entire process. Upstream process modifications can have a great impact on the drying stage, whereas the method of drying is often of paramount importance to product quality.

Procedures for determining the optimum dryer to use are covered in Chapter 3. One scheme is presented for continuous dryers, with a separate scheme for batch dryers. Chapter 4 provides an introduction to convective drying, and Chapters 5 through 8 cover in detail the four main categories of convective dryers. In these chapters, the performance of dryers is analyzed, their literature data interpreted, and design methods are covered. The material that is presented permits an estimation of both fixed and relevant variable costs for convective dryers. In Chapter 9, miscellaneous continuous convective dryers and convective batch dryers are discussed, and atmospheric contact dryers are treated in Chapter 10. Vacuum drying, including freeze-drying, is covered in Chapter 11. Steam drying is treated in Chapter 12. Radiation drying (infrared, radio-frequency, and microwave drying) is dealt with in Chapter 13, and the important issues of product quality and safety are considered in Chapter 14. Fires and dust explosions are treated in the context of safety. Chapter 15 covers continuous solids- and gas-moisture measurement, dryer process control, and energy recovery.



Figure 1.1 Drying tower for madder roots. (Courtesy of Streekmuseum voor Tholen en Sint-Philipsland "De Meestoof", Sint-Annaland, The Netherlands.)

The separation of particulate solid material from spent drying gas by means of cyclones, fabric filters, scrubbers, and electrofilters are the topics in Chapter 16, and the selection of feeders for dryers is taken up in Chapter 17.

One hundred and fifty years ago, drying was often a very time-consuming process. We illustrate this by means of an example, the manufacture of a red dye from madder roots. Madder is a plant with long, thick roots that contain a red dye. From possibly 1400 until approximately 1900, this dye was manufactured industrially in Great Britain and The Netherlands. The roots were harvested and, as a first step, dried in a drying house (see Fig. 1.1). The roots were first laid on the lowest floor and were moved to higher floors as the drying proceeded. An oven at ground level heated the drying house. Control of the drying process was as follows:

- More or less intense fire
- Deposition of stones on the bottom ducts
- Degree of opening of the hatches at the top

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The roots contained approximately 80% water by weight. A typical plant's annual capacity amounted to 100 metric tonnes, with a water evaporation of 400 metric tonnes. The installation of steam tubes around 1850 made possible a more reproducible drying process. The latter meant a switch from convective drying to contact drying. The first drying step was followed by a postdrying step on an oast and a milling step. The practice of manufacturing the red dye from madder was stopped around 1900 because in 1868, Gräbe and Liebermann discovered the synthesis of alizarine from anthracene, and alizarine could replace the red madder dye.

In general, contact drying in steam-heated rotary dryers began in 1830. The development of convective drying began in 1890 when cheap electromotors to drive air fans became available. Spray drying began between 1920 and 1930. Freeze-drying dates back to 1935, and microwave drying was introduced in 1955.

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